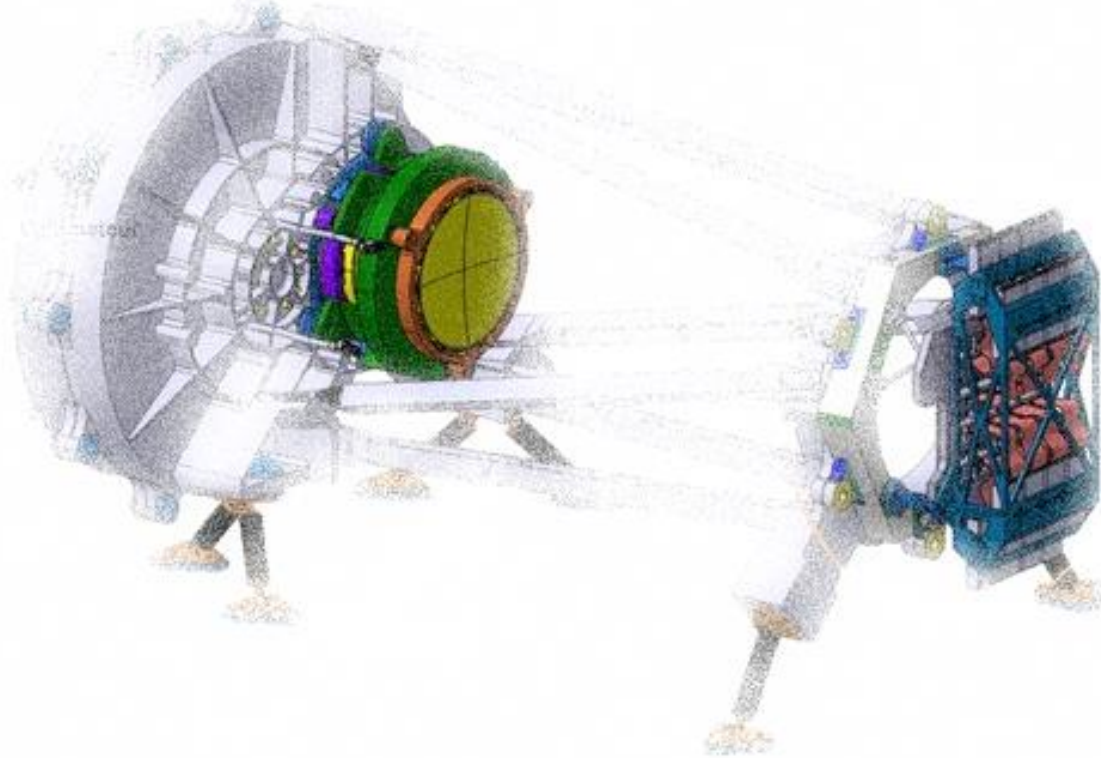


# 3D metrology inside a vacuum chamber with a laser tracker for NISP test campaign

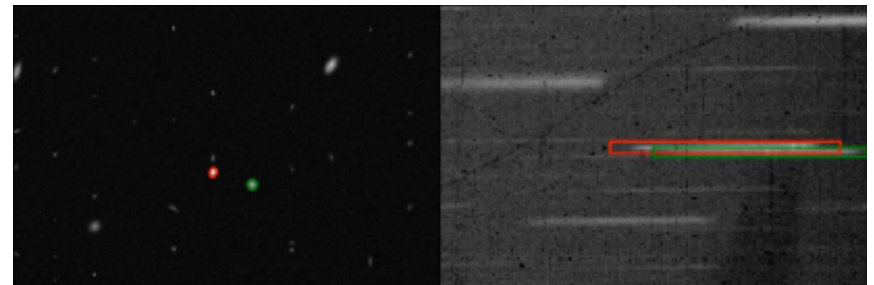
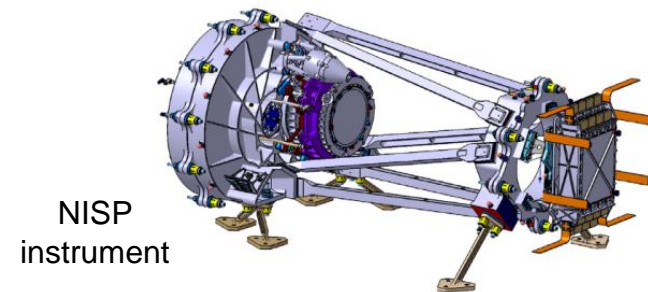
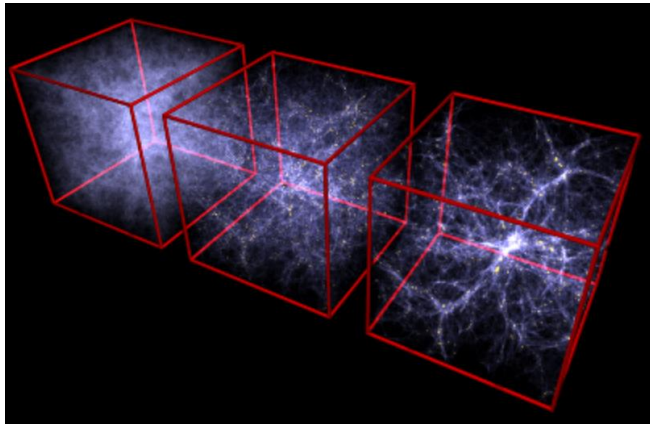
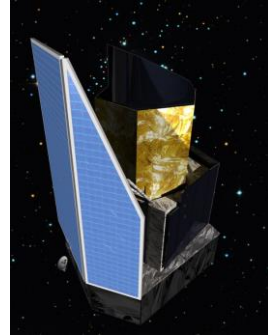
A. Costille, F. Beaumont, E. Prieto, M. Carle, C. Fabron  
Symetrie company for all tests with the mechanical standard



GRD seminar  
08/02/2018

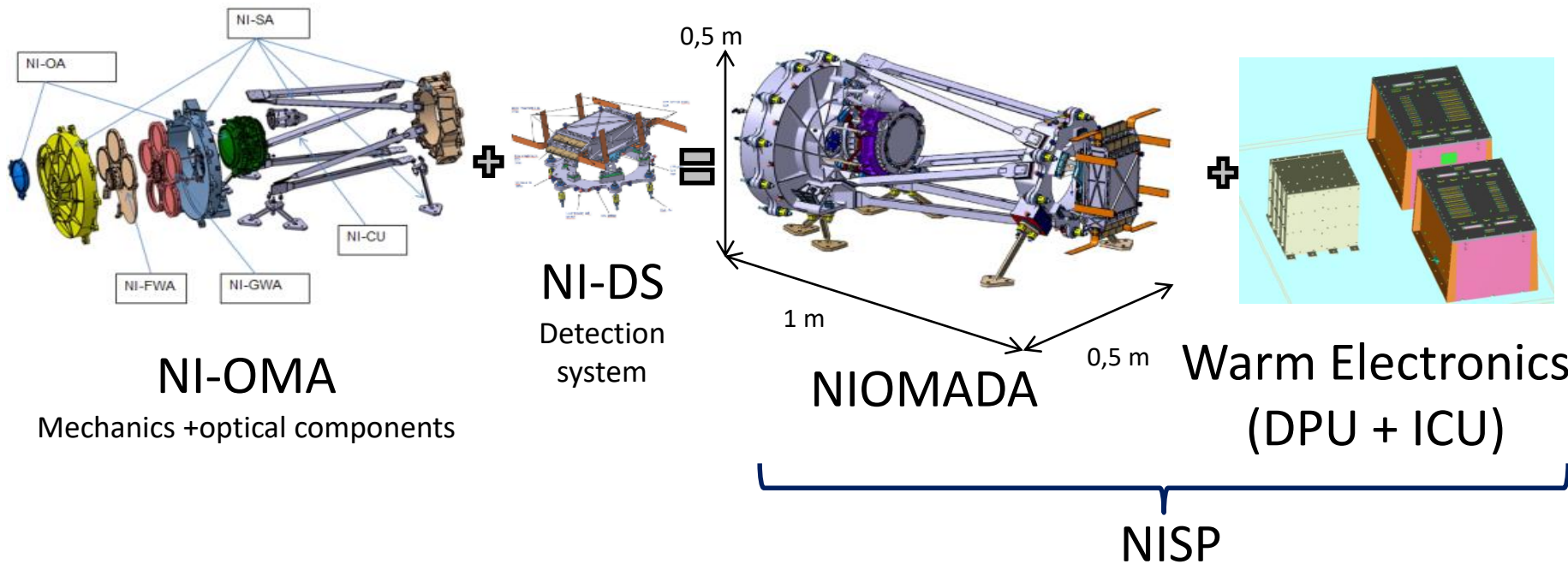
1. EUCLID mission and NISP instrument
2. NISP performance test campaign  
Goal and description of ERIOS configuration  
Description of the hardware and GSEs for NISP TB/TV
3. Metrology needs for NISP TB/TV
4. Metrology verification plan
5. Test campaign results

- EUCLID mission: scientific goals
  - Study of the dark matter distribution and the dark energy in the universe
  - 3D map of the geometry of the dark universe
- Science done with 2 instruments:
  - The VIS imager: visible instrument for photometry of the galaxies in the Visible
  - The NISP: Near Infrared Spectro-Photometer: NIR instrument for
    - ✓ Photometry of the galaxies: position in 2D
    - ✓ Spectroscopy to know precisely the redshift of the galaxies: position in time



Credit J.  
Zoubian

- NISP instrument is made by a consortium of more than 6 countries
  - Project manager of the project is from CNES
  - LAM is responsible of the **development, assembly and test** of the instrument
  - LAM is providing several sub-systems of the instrument: NI-SA, NI-GR, NI-TC
- Instrument will be delivered to ESA in June 2019 (date to be confirmed)

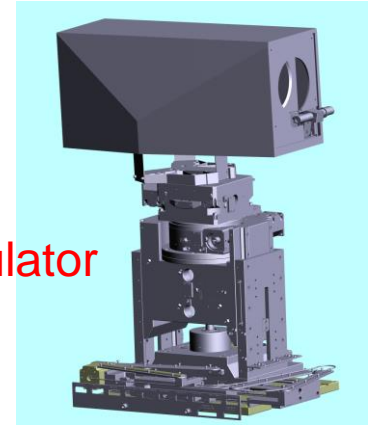


- NISP instrument will be fully tested at LAM

- Functional tests:

- ✓ Motors movement at cold (filter and grism wheel)
    - ✓ Detector acquisition at cold
    - ✓ NISP thermal behavior at cold

Telescope simulator  
needed



- ⊙ Performance tests:

- ✓ Detector characterisation at cold with warm electronics
      - Dark, noise, intra-pixel response, linearity, latency, pixel non homogeneity
    - ✓ Optical characterisation at cold
      - FoV verification, plate scale, optical quality (encircled energy)
      - Rough measurement: througput, stray light (verification no big problem)
      - Spectral dispersion full characterisation

- ⊙ Optical interfaces with PLM verification at cold

- ✓ Object plane measurement
    - ✓ Optical axis measurement

ERIOS chamber needed



- ⊙ Validation of the calibration strategy at cold

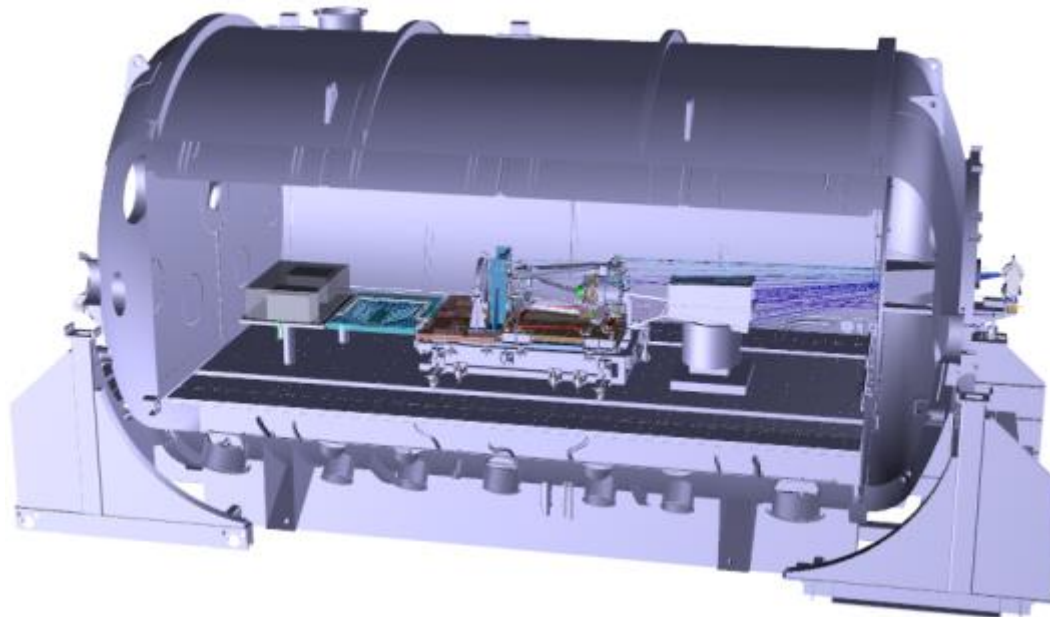
- ⊙ Observation strategy test at cold

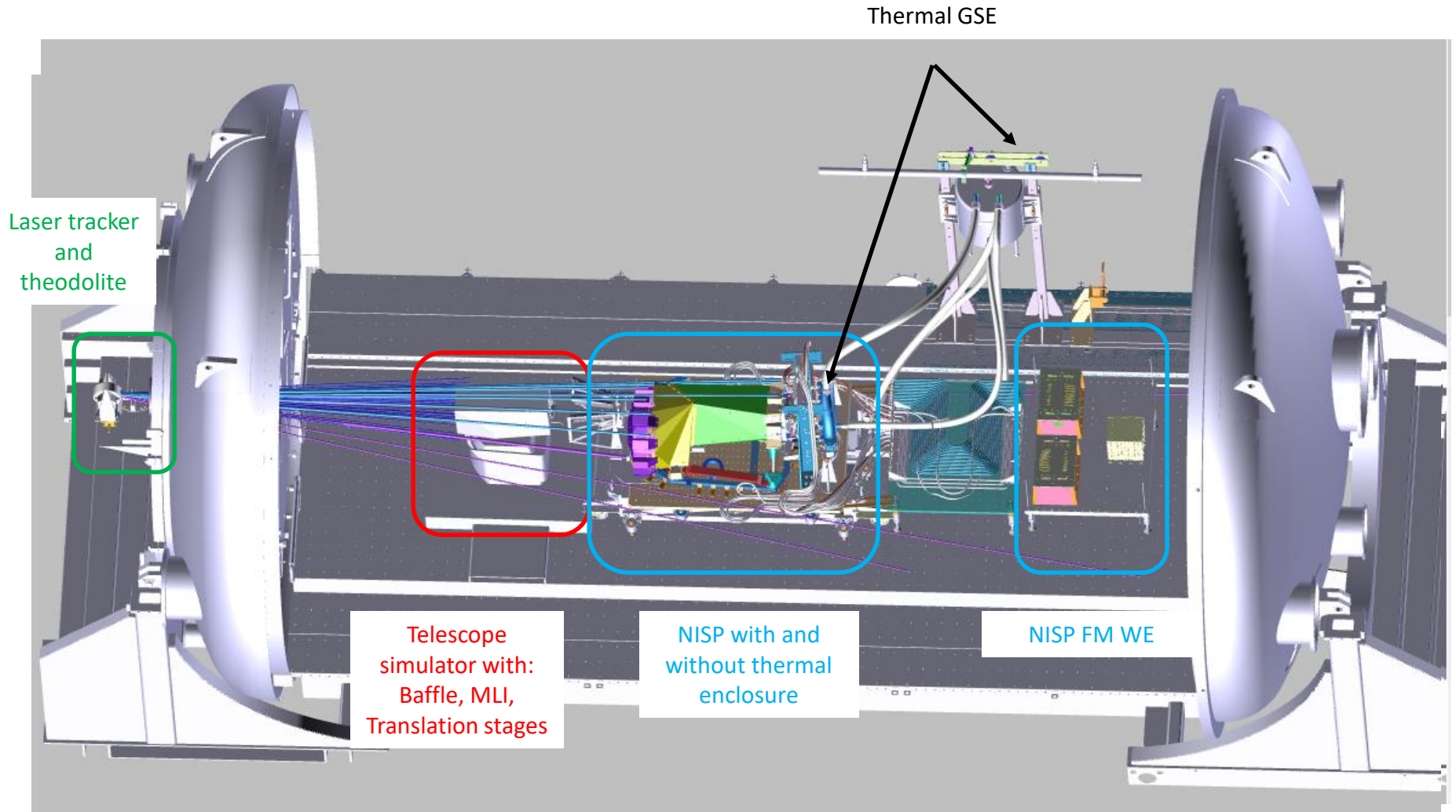
Laser tracker  
needed



- A global mean called the Verification Ground Support (VGS) has been developed for NISP test
- It contains:
  - Optical means (OGSE) with a telescope simulator
  - Thermal and Mechanical means (MGSE & TGSE) to put and maintain the instrument at operational temperature
    - ✓ 130K for the structure, 90K for the detector with a stability lower than 4mK on detectors
  - Metrology mean to measure the positions of the items in real time at cold and vacuum

Inside ERIOS  
vacuum  
chamber





- Design and development of the different GSE is on going:
  - Validation of the metrology in vacuum: **done in September 2017**
    - ✓ Will be presented in next slides
  - Validation of the thermal and mechanical interfaces: **done in December 2017**
  - Test and assembly of the OGSE: on going work done by a Danish team
    - ✓ Delivery at LAM in March 2018
    - ✓ Complete test in ERIOS at cold: April 2018
- Today planning for NISP TB/TV test :
  - Engineering model Test : only mechanics, electronics and software. No optics: July 2018
  - NISP first TB/TV : NISP instrument with non Flight model detector electronics: October 2018
    - ✓ First optical validation, partial characterisation
  - NISP second TB/ TV: characterisation of the NISP detector with Flight Model detector electronics : January 2018 (TBC)
  - NISP vibration test: March 2018 (TBC)
  - NISP final TB/TV : full performance and functional characterisation of NISP instrument before delivery to the payload: May 2018 (TBC)



CSS LN2 Tank

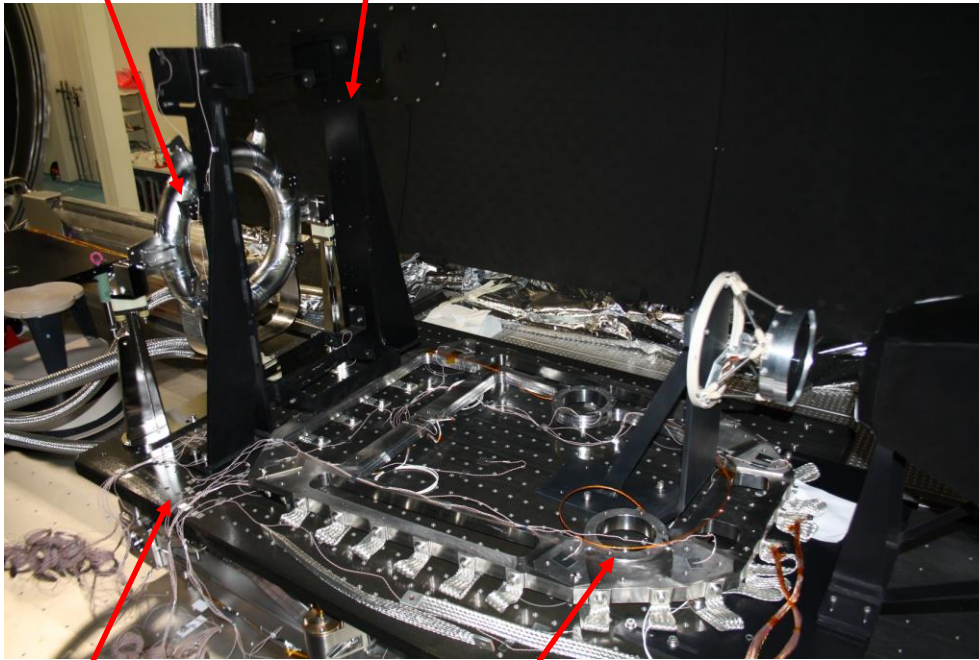
NIDS connector harness ark

Interface for CPPM detector

NISP Auxiliary tank

WE interface

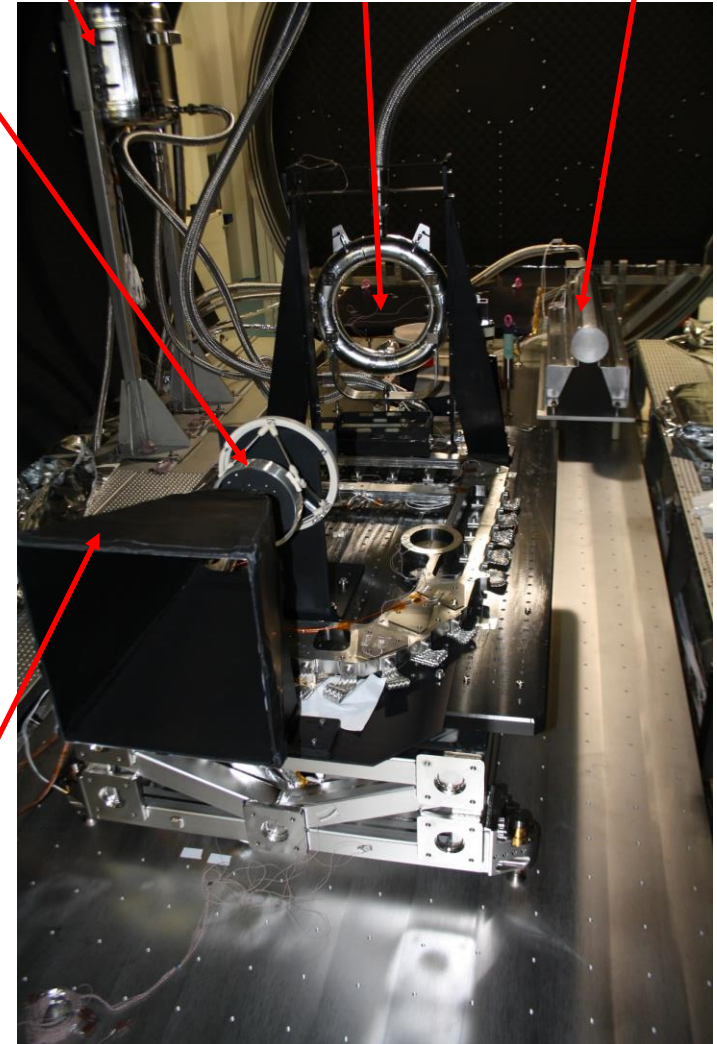
Cold trap for WE

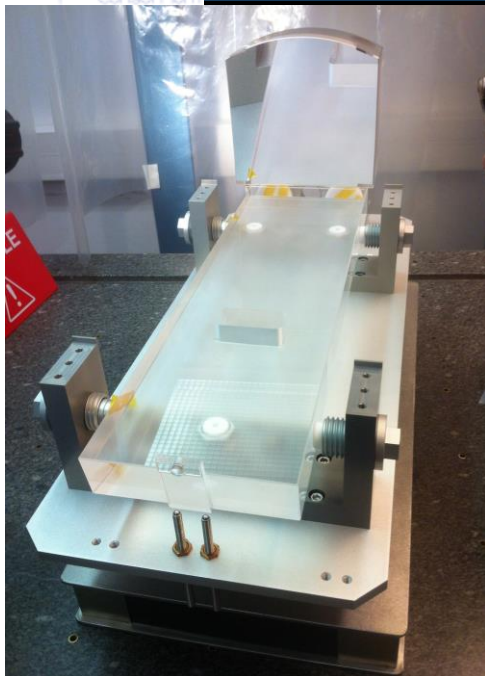


Cold plate

NI-TF: Mechanical interface for NISP feet

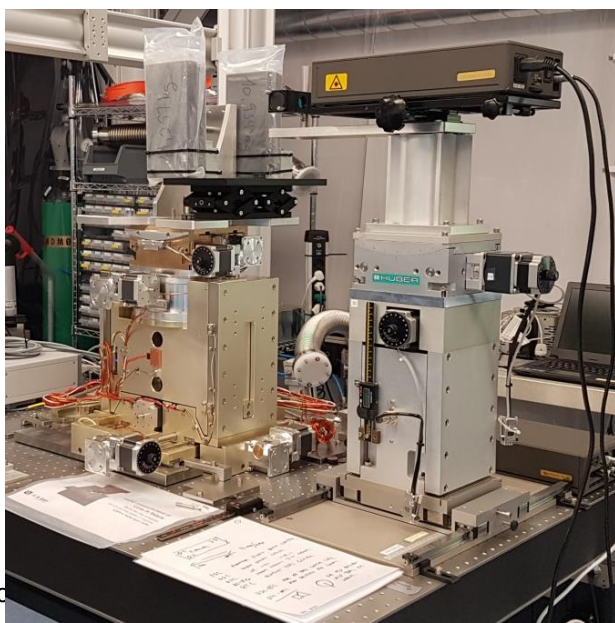
NISP-telescope simulator baffle



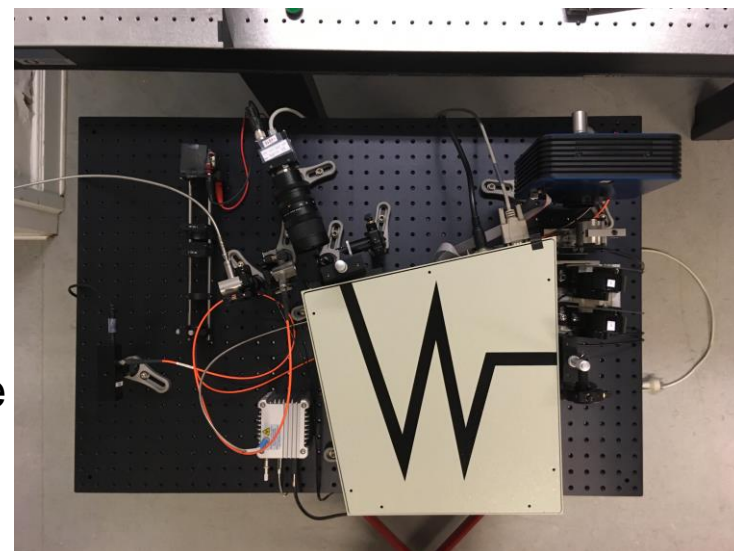


**Telescope simulator :**  
off axis parabola of 160mm diameter  
On back-side : small mirrors for  
theodolite measurement

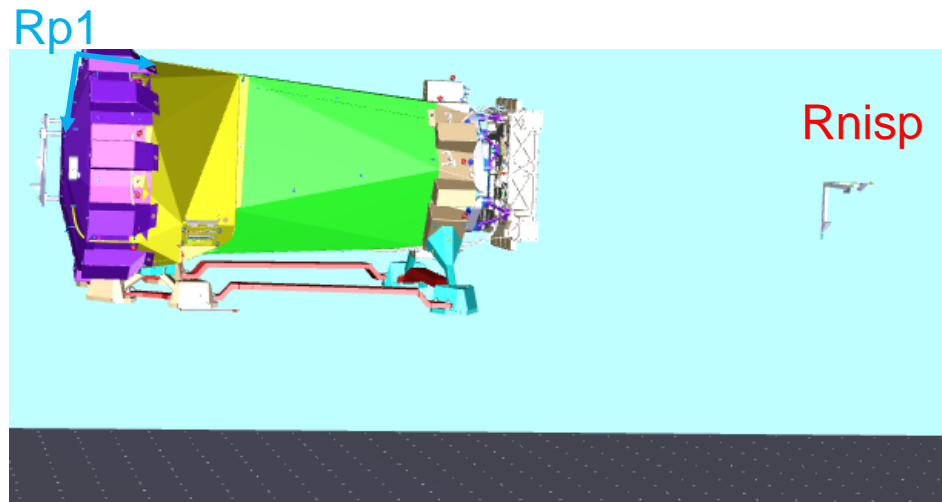
Light source module  
(outside erios)



Translation stages  
under the telescope  
simulator

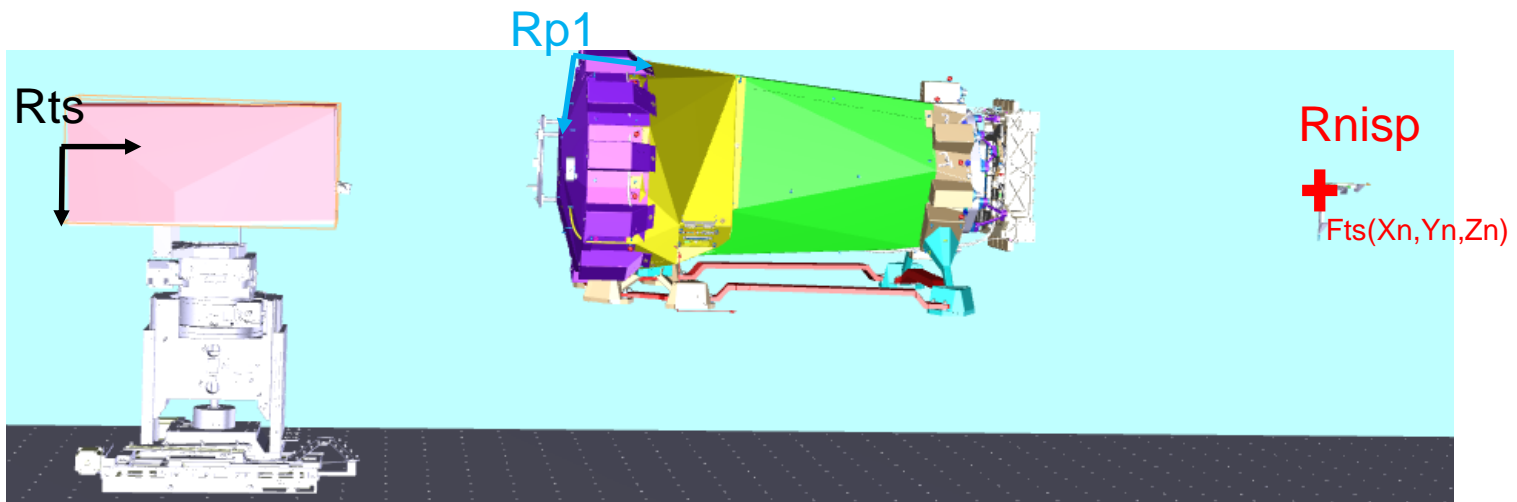


- Goal of the metrology for NISP TB/TV:
  - To measure the best focus plane of NISP instrument with respect to NISP reference frame
  - NISP reference frame = attached to object plane of EUCLID telescope  
= optical interface between NISP and EUCLID telescope
    - ✓ Need to be simulated during the TB/TV test



The telescope simulator (OGSE) will simulate the focus object of Rnisp  
 $F_{TS}(X,Y,Z)$  during the test for one point of the field

- How do we do ? We measure the relative position of reference frames:
  - $R_{TS}$ : reference frame on the telescope simulator
  - Knowledge of  $R_{TS}$  provides the knowledge of the object focal point of EUCLID
 
$$R_{TS} = M_{TS} \times F_{TS}$$
  - $R_{P1}$ : NISP reference frame that is linked to NISP detector plane through metrology done at NISP instrument level
- The telescope simulator is focused on 1 point of the NISP FoV
  - We measure **We need to measure the position of reflectors at cold**
- We repeat this process for all points of the NISP FoV
- We calculate the best focus plane



- A laser tracker:
  - Portable coordinates measuring machine provided by LEICA
  - Allow extreme accuracy over large distances
  - It is an accurate theodolite combined with an accurate measuring equipment

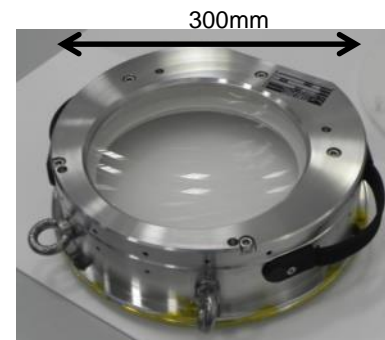
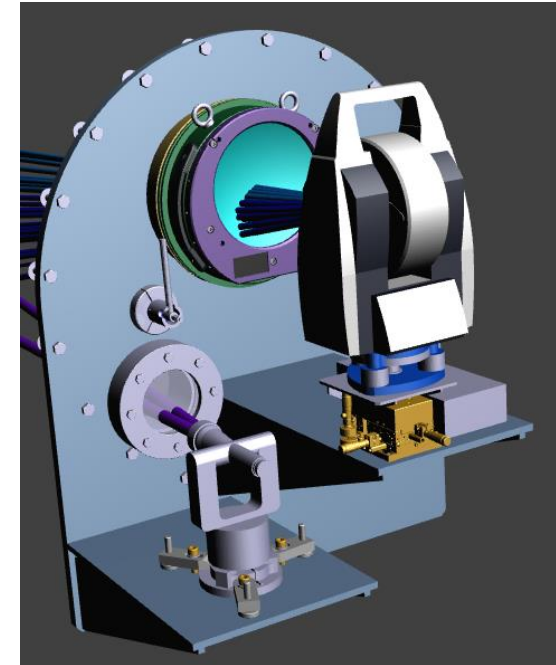


Minimal distance of use	1.5m
Maximal distance of use	> 50m
On axis measurements	
Resolution	0.001mm
Accuracy	0.002mm
repeatability	0.001mm
3D measurements	
Angular accuracy	0.001°
Angular resolution	0.001°
repeatability	0.001°
	0.001mm + 3µm /m

**Not compatible with vacuum and cold temperature**

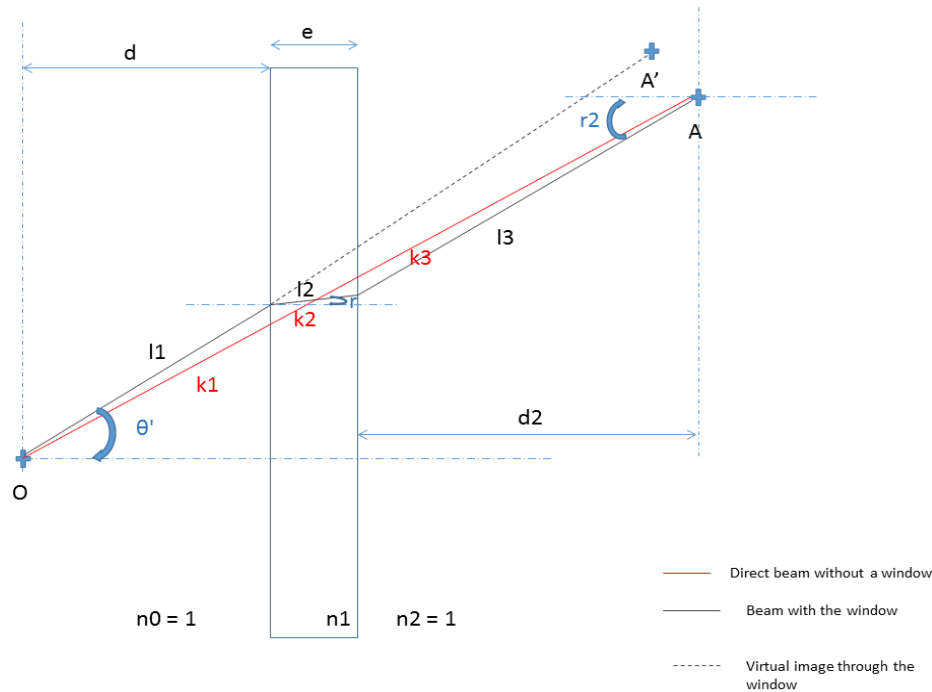


- For NISP need:
  - The laser tracker is installed outside ERIOS in front of a window of 180mm clear aperture (35mm thick)
- For the measurement, the laser tracker measures:
  - The return signal from the reflectors (polarimetric signal)
  - Temperature, Pressure, Humidity of the environment to calculate the air index
  - The reflectors will be installed on NISP and TS inside ERIOS (Pvacuum, cold temperature)
- BUT :
  - The laser tracker « does not know » that there is between the reflector and the measurement sets:
    - ✓ A window with index  $n_v$
    - ✓ A « vacuum » and cold environment



- To validate the use of the laser tracker, we have to answer several questions:
  - Is a measurement possible through a window ? **Yes (test done in early 2016)**
  - What type of window should be used ? **Plane or curved window ?**
    - ✓ How the measurement is disturbed by the window ?
    - ✓ What is the impact of the position between the laser tracker and the window ?
    - ✓ What is the error added by the window ?
    - ✓ How do we correct the measurement done ?
  - Is a measurement possible if the laser tracker is installed directly on ERIOS chamber door ? **Study during NISP metrology system test campaign**
    - ✓ If yes, what is the impact of the vibrations from ERIOS ?
    - ✓ How the position between the window and the laser tracker is disturbed by ERIOS environment
    - ✓ What is the impact on the window of ERIOS environment (vacuum, cold) ?
  - How the reflectors behave at cold ? **They survive (test done in early 2016)**
    - ✓ If yes, what is the impact on the measurement error ?
  - **What is the measurement error ?**

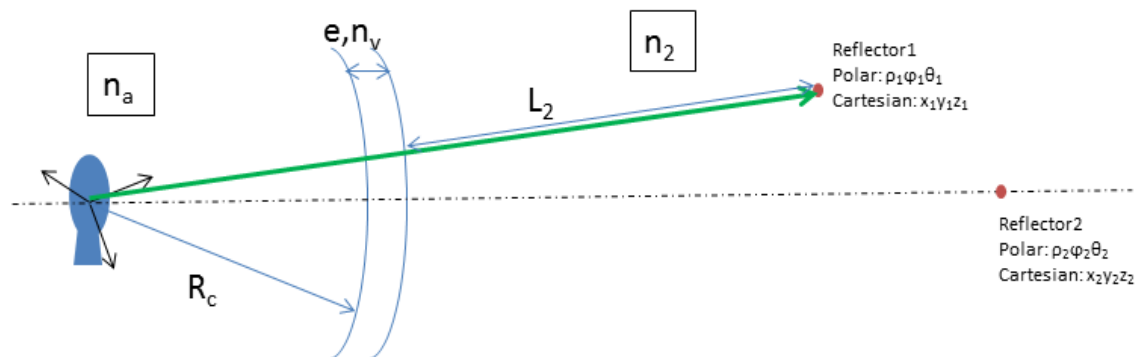
- 2 solutions are possible:
  - Use a classic parallel plate as a window
    - ✓ The window will move the object position from the laser tracker
    - ✓ 3D equations of the light propagation should be written to correct the measurement done by the laser tracker





- 2 solutions are possible:
  - Use a classic parallel plate as a window
    - ✓ The window will move the object position from the laser tracker
    - ✓ 3D equations of the light propagation should be written to correct the measurement done by the laser tracker
  - Use a « curved » window = concentric concave surfaces
    - ✓ If the laser tracker is placed at the center of curvature of both faces, the beam is not deviated by the window
    - ✓ The error on the measurement will only be on the distance measurement, not on the angular position
    - ✓ Using light propagation time, we calculate the following correction law:

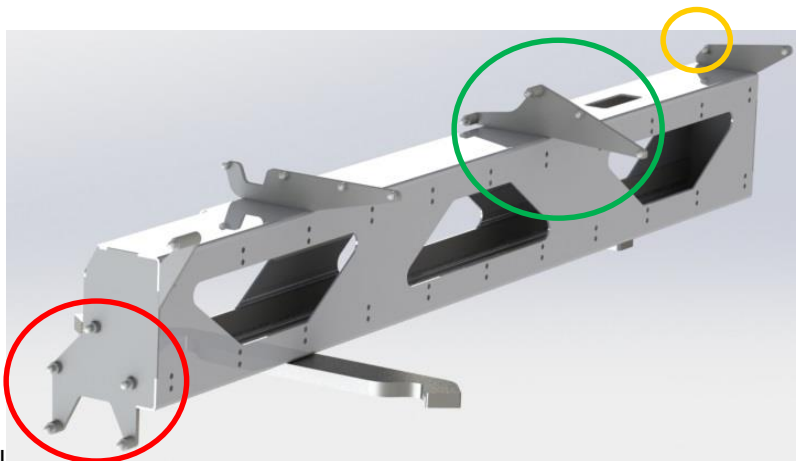
$$L = Rc + e + L_2 = \frac{n_a}{n_2} L_m + Rc \left(1 - \frac{n_a}{n_2}\right) + e \left(1 - \frac{n_v}{n_2}\right)$$



- Goal of the verification plan is to demonstrate the feasibility and the performance of the metrology for NISP test
  - What accuracy can be reached for measurement at cold and vacuum with a laser tracker ?
- Preliminary tests have shown that the main impact of the laser tracker errors was:
  - The window
  - The vacuum
  - Impact of cold temperature was negligible
- It has been decided to focus the verification strategy on effect of vacuum
  - Adding test at cold was too restrictive

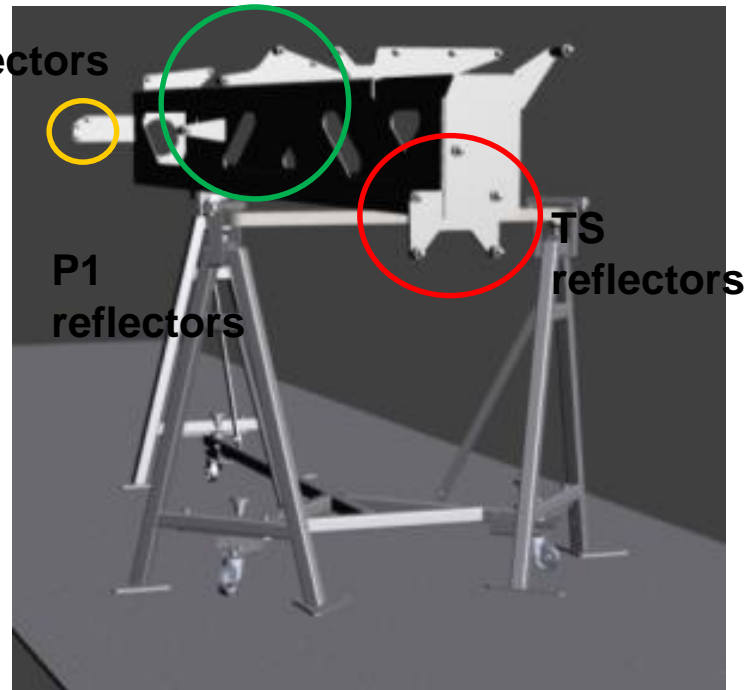
- Verification plan strategy
  - To have a standard mechanical part representative of the NISP TB/TV test configuration to know what we are measuring
  - To perform a sequential analysis
    - ✓ Knowledge of the frame
    - ✓ Measurement of the frame with a laser tracker no window
      - Estimation of the laser tracker uncertainties
    - ✓ Measurement of the frame with a laser tracker through the curved window
      - Estimation of the error introduced by the window
    - ✓ Measurement of the frame with a laser tracker through the curved window in vacuum in ERIOS
      - Estimation of the error introduced by the vacuum and ERIOS conditions
    - ✓ Measurement during VGS blank test at cold
      - Validation that the cold is not added errors on the measurement
- Work has been done in collaboration with Symetrie company

- Symetrie company was in charge of:
  - The design of the mechanical standard
  - The measurement and analysis of the mechanical standard with:
    - ✓ The CMM
    - ✓ The laser tracker
    - ✓ The curved window: work done in collaboration with LAM for alignment and measurement with the window
- The mechanical standard reproduces:
  - TS reflectors positions
  - P1 and P3 reflectors positions
  - other planes has been added for analysis
- Design of the mechanical standard ensures its stability with temperature and time

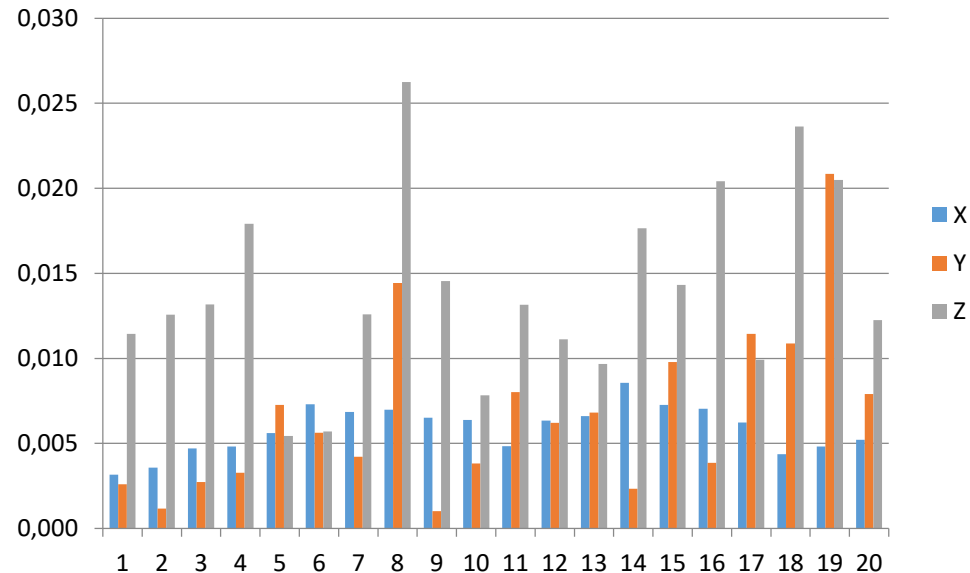


**P3**

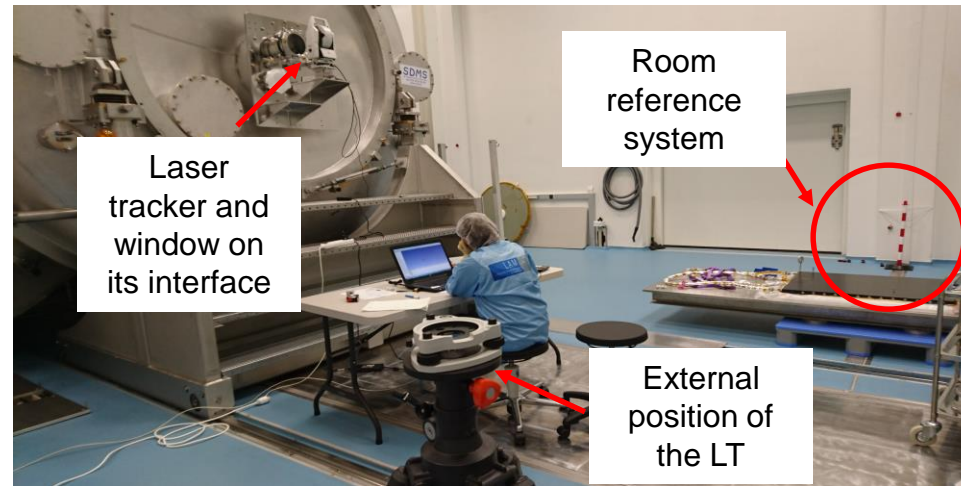
**reflectors**



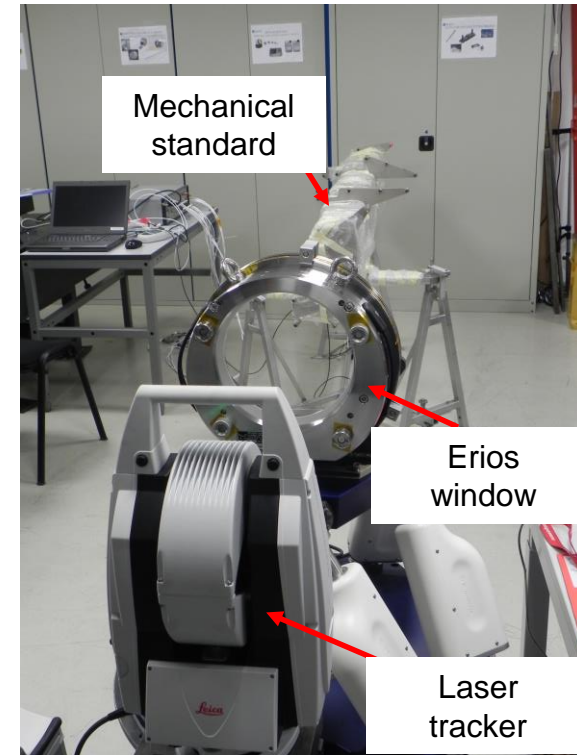
- Measurement of the mechanical standard with a CMM
  - Definition of a reference system on the mechanical standard Ret to locate precisely position of each reflector on the frame: (X0, Y0, Z0)
  - Measurement uncertainties:  $13,2\mu\text{m} + 1,8^{\text{e}}-6\text{L}$
- Measurement with the laser tracker without a window
  - To estimate error budget from the laser tracker alone
  - Uncertainties of the reflectors positions is different from the axis measured
    - ✓ Better uncertainty reached for measurement in X direction (optical axis): better than  $10\mu\text{m}$
    - ✓ Lower uncertainty reached for measurement in Y and Z direction: around  $20\mu\text{m}$
  - Measurement uncertainties:  $62\mu\text{m} + 2,7^{\text{e}}6\text{L}$



- Alignment between the laser tracker and the curved window on the window curvature center
  - Metrology of the window is done
    - ✓ A cartesian coordinate system is defined to locate the center of curvature  $R_w$
  - The LT locates  $R_w$  in a room reference system
  - Laser tracker is installed on its interface and move to align the laser tracker center on  $R_w$  in the room reference system
  - Alignment better than  $300\mu\text{m}$  is reached



- Measurement of the mechanical standard with the laser tracker through the window
  - Coordinates (X2, Y2, Z2) for each reflectors in Ret
  - In spherical coordinates, a constant error in distance is measured: 13,93mm
    - ✓ Consistent with the impact of the glass:  $d = e(nv-na)$
  - Coordinates (X3, Y3, Z3) are calculated with constant error correction
  - Difference between (X3, Y3, Z3) and (X0, Y0, Z0) is calculated
  - Difference better than 30μm (mean values on each reflectors coordinates)



$(\rho_2, \theta_2, \phi_2) - (\rho_0, \theta_0, \phi_0)$

Bille #	$\Delta\rho$ (mm)	$\Delta\theta$ (°)	$\Delta\phi$ (°)
BILLE_1	13,929	-0,005	-0,009
BILLE_2	13,925	-0,005	-0,010
BILLE_3	13,924	-0,005	-0,009
BILLE_4	13,927	-0,005	-0,009
BILLE_5	13,926	-0,005	-0,009
BILLE_6	13,925	-0,005	-0,009
BILLE_7	13,930	-0,005	-0,009
BILLE_8	13,930	-0,005	-0,009
BILLE_9	13,928	-0,005	-0,009
BILLE_10	13,928	-0,005	-0,009
BILLE_11	13,927	-0,005	-0,009
BILLE_12	13,930	-0,005	-0,009
BILLE_13	13,929	-0,005	-0,009
BILLE_14	13,931	-0,005	-0,009
BILLE_15	13,934	-0,005	-0,009
BILLE_16	13,940	-0,005	-0,009
BILLE_17	13,940	-0,004	-0,009
BILLE_18	13,933	-0,005	-0,009
BILLE_19	13,931	-0,004	-0,009
BILLE_20	13,936	-0,004	-0,009

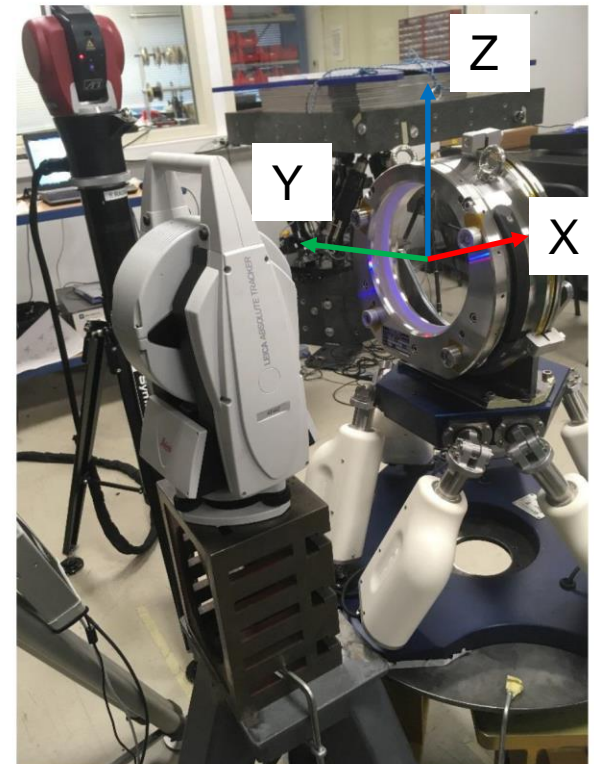
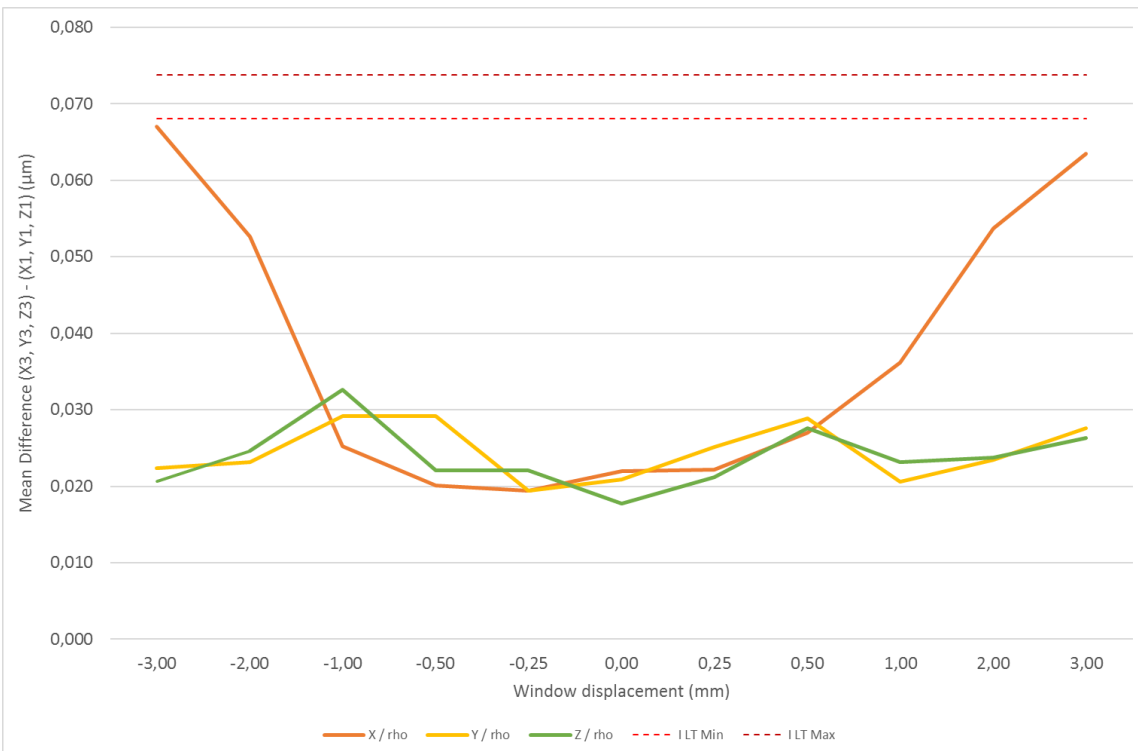
Min	13,924	-0,005	-0,010
Max	13,940	-0,004	-0,009
Moy	13,930	-0,005	-0,009
Ecart Type	0,005	0,000	0,000

$(\rho_3, \theta_3, \phi_3) - (\rho_0, \theta_0, \phi_0)$

Bille #	Correction $\rho$			Correction $\rho \theta \phi$		
	$\Delta X$ (mm)	$\Delta Y$ (mm)	$\Delta Z$ (mm)	$\Delta X$ (mm)	$\Delta Y$ (mm)	$\Delta Z$ (mm)
BILLE_1	0,015	0,034	-0,005	0,015	0,029	-0,005
BILLE_2	0,016	-0,003	0,031	0,016	-0,007	0,030
BILLE_3	0,011	0,023	0,015	0,011	0,021	0,016
BILLE_4	0,012	0,014	0,017	0,012	0,013	0,017
BILLE_5	0,010	0,025	-0,006	0,010	0,025	-0,005
BILLE_6	0,005	0,013	-0,012	0,005	0,013	-0,012
BILLE_7	0,004	0,019	-0,013	0,004	0,019	-0,014
BILLE_8	0,000	0,000	0,000	0,000	0,000	0,000
BILLE_9	0,004	-0,005	0,000	0,004	-0,005	0,001
BILLE_10	0,000	-0,011	0,000	0,000	-0,011	0,000
BILLE_11	0,003	-0,021	0,023	0,003	-0,023	0,022
BILLE_12	0,001	0,000	0,014	0,001	-0,001	0,014
BILLE_13	-0,004	-0,008	0,006	-0,004	-0,008	0,006
BILLE_14	-0,003	-0,008	-0,013	-0,003	-0,008	-0,013
BILLE_15	0,000	-0,005	-0,007	0,000	-0,004	-0,008
BILLE_16	0,000	0,000	0,000	0,000	0,000	0,000
BILLE_17	-0,001	0,035	0,013	-0,001	0,034	0,014
BILLE_18	-0,002	0,028	0,023	-0,002	0,026	0,023
BILLE_19	-0,008	-0,011	0,040	-0,008	-0,013	0,040
BILLE_20	0,003	0,023	0,025	0,003	0,021	0,025

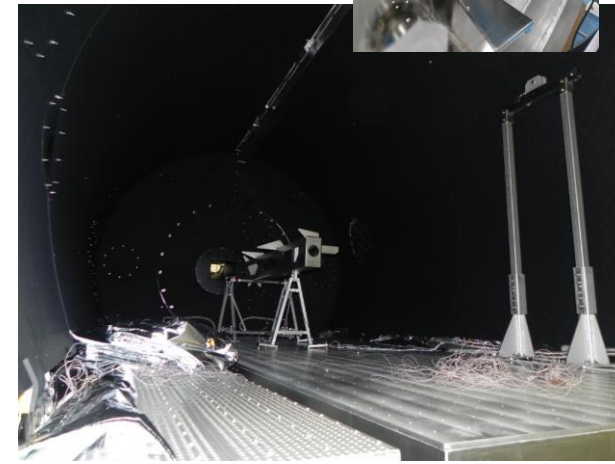
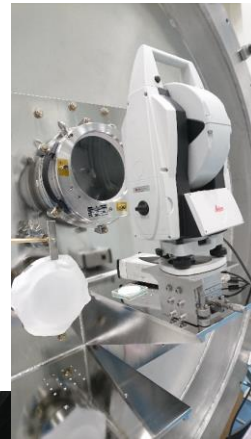
Min	-0,008	-0,021	-0,013	-0,008	-0,023	-0,014
Max	0,016	0,035	0,040	0,016	0,034	0,040
Moy	0,003	0,007	0,008	0,003	0,006	0,008
Ecart Type	0,006	0,017	0,016	0,006	0,017	0,016

- Sensibility analysis done between the position of the window and the laser tracker
  - Window is moved in each direction of  $\pm 3\text{mm}$
  - Impact of the difference is calculated
  - Error added by the window is lower than  $30\mu\text{m}$  when the laser tracker is aligned around  $\pm 1\text{mm}$  from the curvature center
  - More impact if we move along the optical axis of the window





- Test of the MVS at Pvacuum and Tambient is Erios has been done in September 2017:
  - The mechanical standard has been installed inside ERIOS
  - Reflectors coordinates are compared to the value of the measurement standard coordinates on the CMM
- This test has allowed:
  - Validating the alignment procedure of the laser tracker with the curved window
  - Validating of the correction factor to be applied to the data at Pambient and Pvacuum
  - Estimating the measurement uncertainties at Pvacuum



- With the window alone, impact on the laser tracker measurement
  - Error of 13,93mm in the distance measurement (in spherical coordinates)
  - Impact on angle measurement values negligible ( $\theta, \phi$ )
- Hypothesis taken for the impact of the vacuum on the laser tracker measurement
  - Error on the distance measurement linked to:
    - ✓ The window
    - ✓ The vacuum index (=1)
  - Impact on angle measurement values negligible( $\theta, \phi$ )
  - The laser tracker is aligned on the window curvature center better than +/-1mm
- We propose to apply the correction factor:

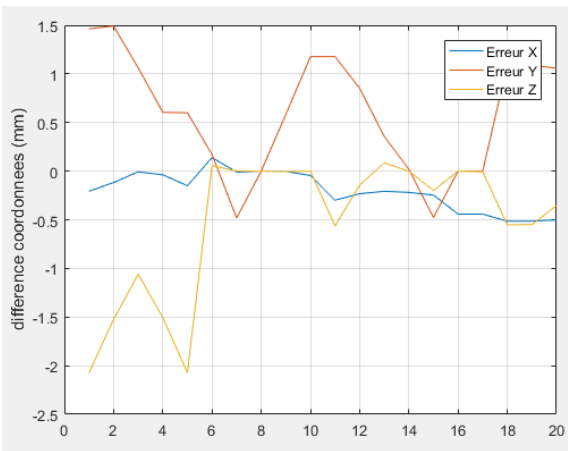
$$\rho_{\text{corr}} = \rho_{\text{mes}} - 13.93\text{mm} + (n_a - 1) * (\rho_{\text{mes}} - 13.93 - 300)$$

- Analysis done with the comparison of the reflectors coordinates measured with the laser tracker and a CMM

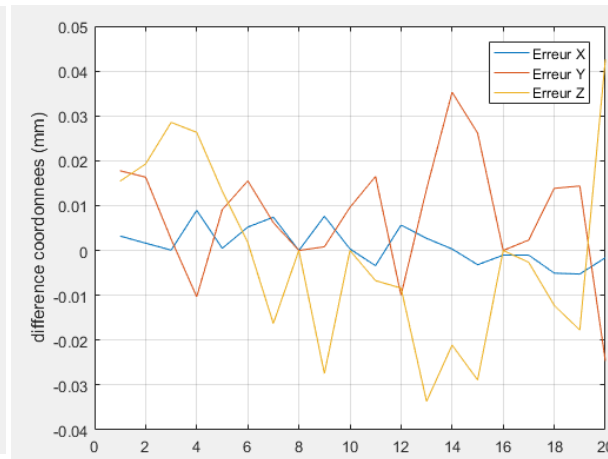
- Coordinates difference in (X,Y,Z)

$$diff = \sqrt{(x_{lt} - x_{CMM})^2 + (y_{lt} - y_{CMM})^2 + (z_{lt} - z_{CMM})^2}$$

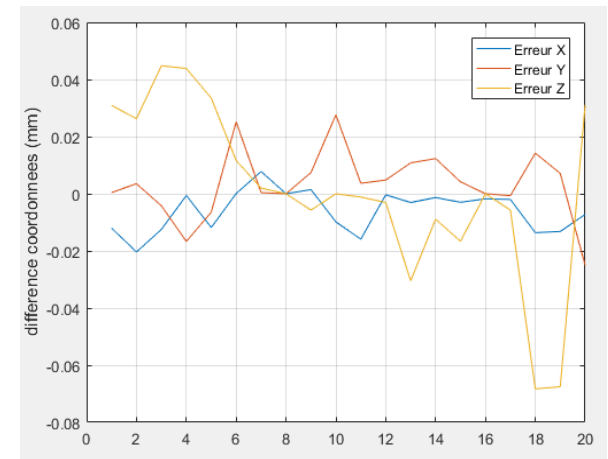
- Residual Error on the coordinates lower than 60µm ie lower than measurement uncertainties



No correction of the data

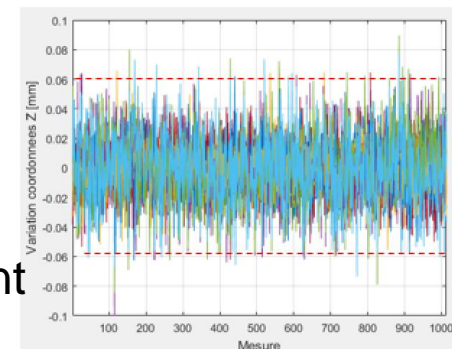
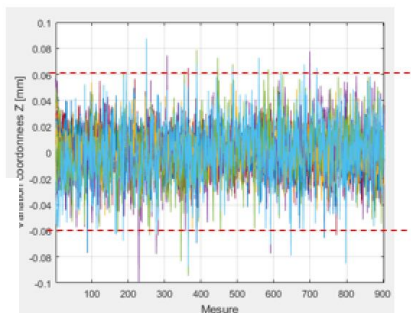
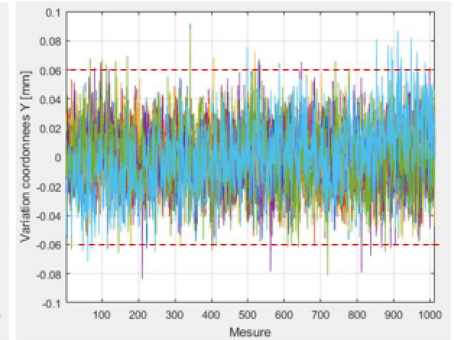
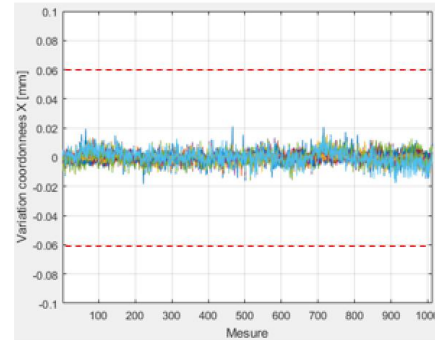
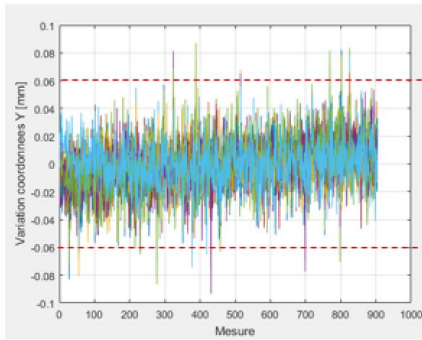
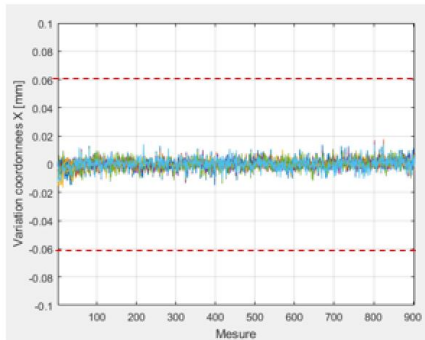


Correction of the data at Pambient



Correction of the data at Pvacuum

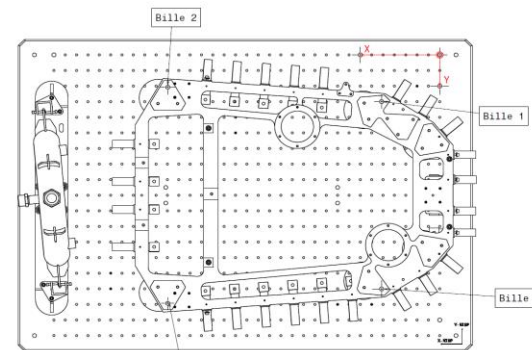
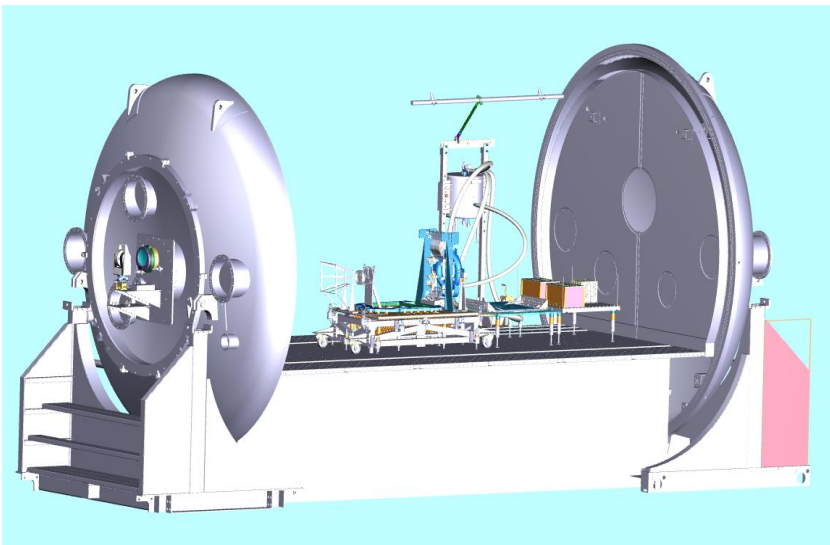
- Measurement repeatability similar at Pambient and Pvacuum
  - Uncertainties on X axis:  $< +/-15\mu\text{m}$ 
    - ✓ Same values as measurement with a laser tracker without a window
  - Uncertainties on Y and Z axis :  $< +/-60\mu\text{m}$ 
    - ✓ Same values as measurement with a laser tracker without a window
  - Small increase of the uncertainties at Pvacuum due to the environment: not critical
- For measurement in Erios, an average of 5 measurements will be considered



Pambient  
measurement

Pvacuum  
measurement

- Additional test has been performed at cold in December 2018
- During the blank test of the thermal and mechanical GSE of NISP, we have put:
  - 3 reflectors on an aluminium plate
  - 4 reflectors on an invar plate (NISP feet interface)
- Goal of the test was:
  - To validate the measurement of reflectors at cold
    - ✓ No deterioration of the reflector due to cold
    - ✓ No measurement issue
    - ✓ No impact of the cryopump on laser tracker measurement
  - To estimate if an additional correction factor is needed at cold

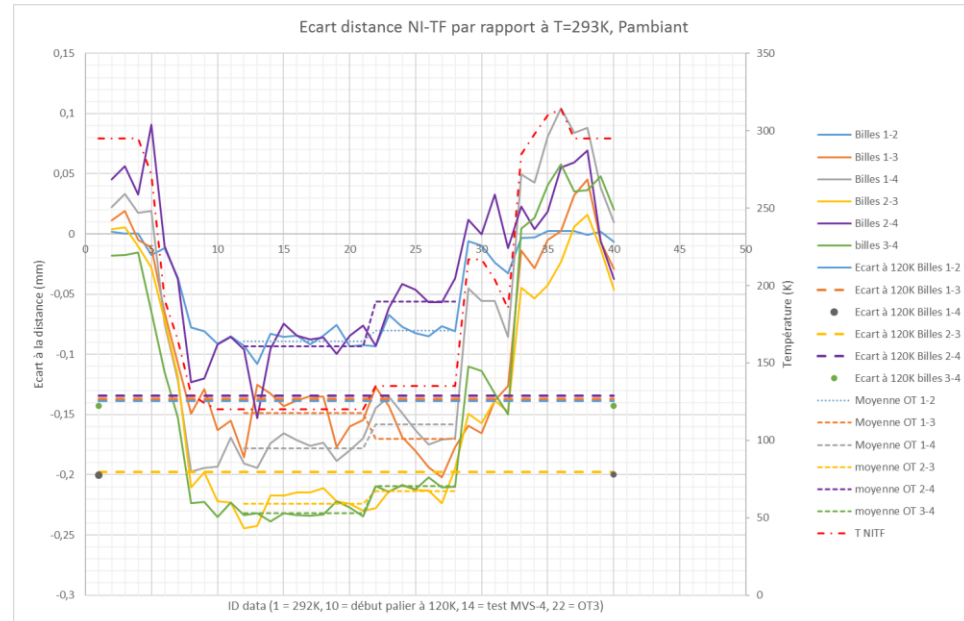
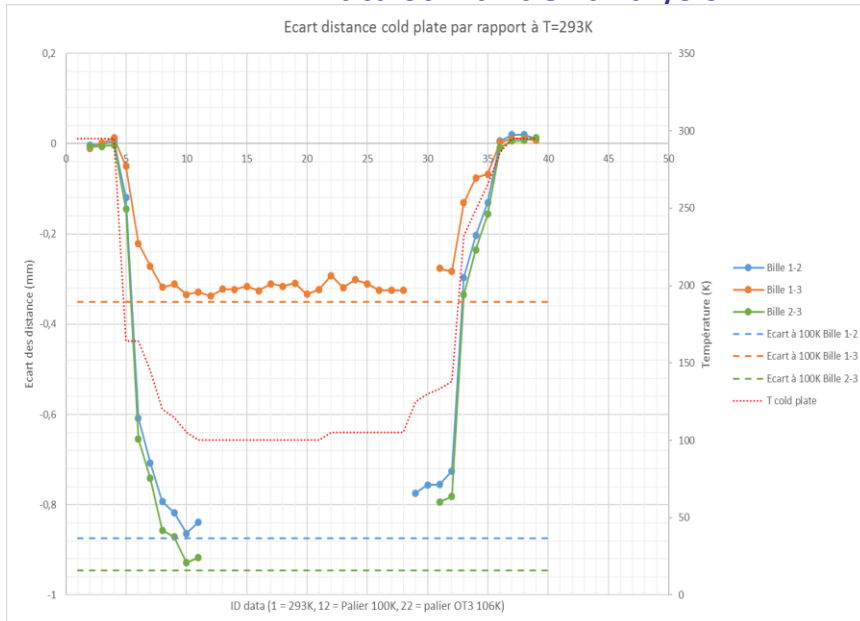


Coordonnées dans  $R_{\text{réf}}$  [mm]:

	Bille 1	Bille 2	Bille 3	Bille 4
X	179.577	149.841	179.577	838.898
Y	55	103.628	750.415	796.629
Z	55	55	55	55

Ref.	Date	Version	Revisé	Statut	Original Issue
1/1					001
Scale: 1/1		Material:		Format: A3	
Mass: kg		Treatment:		NA	
<b>1/1 NISP</b>			TMVS		
Positionnement NI-TF ERIOS			LABORATOIRE D'ASTROPHYSIQUE DE MARSEILLE		
LAM			38, rue F. J. Gaspard, 13288 Marseille Cedex 13		
			Tel: (33) 04 91 88 00 - www.lam.fr		
EUC-GST-60200-IF-A					

- Test was considered as successful as:
  - All reflectors are still « intact » after cold temperature and keep their measurement accuracy
  - Measurement repeatability at cold was similar to the one measured at Pvacuum and Tambient:
    - ✓ Increase of the measurement repeatability with this configuration as the interfaces are less stable mechanically
  - No additional « cold » correction has been identified
    - ✓ Inter-reflector target distance has been measured and compared to estimated cold distance with CTE knowledge
    - ✓ Data still under analysis



- Test campaign done at LAM has demonstrated the feasibility of the laser tracker measurement for NISP TB/TV
  - Is a measurement possible through a window ? **Yes**
  - What type of window should be used ? **Curved window**
    - ✓ How the measurement is disturbed by the window ? **Distance to be corrected by a constant value from the window + variable due to index variation**
    - ✓ What is the impact of the position between the laser tracker and the window ? **Robustness of the alignment has been observed**
    - ✓ What is the error added by the window ? **« nothing » after correction law application**
    - ✓ How do we correct the measurement done ? **Correction law identified**
  - Is a measurement possible if the laser tracker is installed directly on ERIOS chamber door ? **YES**
    - ✓ If yes, what is the impact of the vibrations from ERIOS ? **Increase of measurement repeatability => on X axis < 20 $\mu$ m; on Y and Z axis < 60 $\mu$ m**
    - ✓ How the position between the window and the laser tracker is disturbed by ERIOS environment : **no major impact observed**
    - ✓ What is the impact on the window of ERIOS environment (vacuum, cold) ? **No impact**
  - How the reflectors behave at cold ? **They survive (test done in early 2016)**
    - ✓ If yes, what is the impact on the measurement error ? **Impact lower than the other error term**
  - **What is the measurement error ? Measurement error from the laser tracker at cold and vacuum : +/-80 $\mu$ m (tbc)**

- We have a metrology mean for the NISP TB/TV test campaign
- We have understood the measurement from the laser tracker through a window
- We have developed a method to correct the measurement
- Uncertainties budget still need to be consolidated
  - Will be done thanks to next test campaign
- At the end of NISP test campaign, we will be able to offer this metrology mean for all test campaign done in ERIOS